# Reconciling Haiyan's rate estimate

$$N_{SRC} = N_{HallA} \frac{d\sigma_{SRC}}{d\sigma_{HallA}} \cdot \frac{\Omega_{SRC}}{\Omega_{HallA}} \cdot \frac{\mathcal{L}_{SRC}}{\mathcal{L}_{HallA}} \cdot \frac{\mathcal{L}_{SRC}}{t_{HallA}}$$

$$N_{SRC} = 1900 \cdot (0.092) \cdot (200) \cdot (3.1 \cdot 10^{-4}) \cdot (4.3) = 47$$

My back-of-the-envelope estimate is:

$$N_{SRC} = \frac{d\sigma}{d\Omega_{cm}} \times \Omega_{cm} \times \mathcal{L} \times t$$

$$N_{SRC} = \left(4.0 \cdot 10^{-35} \frac{cm^2}{sr}\right) \times (3.9 \ sr) \times (3.0 \cdot 10^{31} cm^{-2} s^{-1}) \times (4.3 \cdot 10^5 \ s) = 2000$$

#### **Relative Cross Section**

- Hall A's highest data point was at  $s = 11.3 \text{ GeV}^2$ .
- If we assume an 8 GeV beam on a stationary neutron,  $s = 15.9 \text{ GeV}^2$ .
- $(11.3/15.9)^7 = 0.09$

This is not controversial.

## Relative Bin Size

- Assumed factor of 200x increase for GlueX
  - 6 msr for Hall a
  - 1.2 sr for GlueX
- How much is 1.2 sr?
  - $2\pi \cdot [95.5^{\circ} 84.5^{\circ}]$
  - $2\pi \cdot [20^{\circ} 41^{\circ}]$

GlueX will cover a much larger area. It's not clear if this extra area will be less relevant for color transparency.

# **Relative Luminosity**

- Hall A
  - 1.3 x 10<sup>11</sup> photons/s
  - 15 cm liquid deuterium
- GlueX
  - 2 x 10<sup>7</sup> photons/s
  - 30 cm liquid deuterium

Relative factor of 3.1e-4 is not controversial.

## Relative run time

- Hall A's highest kinematics: 28 hours
- GlueX: 5 days = 120 hours

This mixes actual run time (including accelerator inefficiency) with number of scheduled PAC days.

GlueX wall clock time might be 2x larger.

#### Number of Hall A

• Highest Hall A data point had 2.3% statistical uncertainty:

$$N = \frac{1}{(0.023)^2} = 1900$$

(Ignores additional statistical uncertainty from background, etc.)

## Conclusions

I think these rough estimates are reconciled by:

- Solid Angle Coverage
  - 200x ----> 4000x
- Run Duration
  - 4x ----> 8x

50 events \* 20 \*2 = 2000 events

# Relevant numbers

| Solid target | Rad. Length [cm] | Int. Length [cm] | e <sup>–</sup> Density [cm <sup>–3</sup> ] | Density [g/cm <sup>3</sup> ] | Transparency | a2  |
|--------------|------------------|------------------|--|------------------------------|--------------|-----|
| Carbon       | 19.32            | 38.83            | 6.65 E23                                   | 2.21                         | 0.44         | 4.5 |
| Calcium      | 10.42            | 77.31            | 4.67 E23                                   | 1.55                         | 0.29         | 4.7 |
| Iron         | 1.76             | 16.77            | 2.20 E24                                   | 7.87                         | 0.26         | 4.8 |
| Lead         | 0.56             | 17.59            | 2.69 E24                                   | 11.35                        | 0.17         | 4.8 |

Our originally proposed carbon target was:

- 1.9 cm thick
  - 0.07 radiation lengths
  - $1.45E23 C / cm^2$
  - $1.26E24 e^{-}/cm^{2}$
- Divided into 8 foils, each 2.4 mm thick

Expected  $p\pi$ - yield:

- 740 MF events/PAC day
- 230 SRC events/PAC day

# Scenario 1: Replace 1/8<sup>th</sup> total e<sup>-</sup> density with Fe

Iron Target Thickness:

$$\frac{1.26 E24 e^{-}/cm^{2}}{8} \cdot \frac{1}{2.20 E24 e^{-}/cm^{3}} = 716 \,\mu\text{m}$$

$$716 \,\mu\text{m} \cdot 7.87 \,\frac{g}{cm^{3}} \cdot \frac{mole}{56 \,g} \cdot \frac{6E23}{mole} = 6.0E21 \,cm^{-2}$$

Our multi-foil would be:

- $6.0E21 \ cm^{-2}$  Iron
- $1.3E23 \ cm^{-2}$  Carbon

648 MF/day, 201 SRC/day

# Scenario 1: Replace 1/8<sup>th</sup> total e<sup>-</sup> density with Fe

What rates do we expect? Scale from Cabon:

$$R_{Fe} = R_C \cdot \frac{\rho_{Fe}}{\rho_C} \cdot \frac{N_{Fe}}{N_C} \cdot \frac{T_{Fe}}{T_C}$$

I'm ignoring a2 for the moment.

• 
$$R_{Fe}^{MF} = \frac{740}{day} \cdot \frac{6.0E21}{1.45E23} \cdot \frac{30}{6} \cdot \frac{0.26}{0.44} = 90/day$$
  
•  $R_{Fe}^{SRC} = \frac{230}{day} \cdot \frac{6.0E21}{1.45E23} \cdot \frac{30}{6} \cdot \frac{0.26}{0.44} = 28/day$ 

# Summary of Iron Scenarios

#### Events per day

| Event Type | 0/8 <sup>th</sup> $ ho_{e^-}$ Fe | 1/8 <sup>th</sup> $ ho_{e^-}$ Fe | 2/8 <sup>th</sup> $ ho_{e^-}$ Fe | 3/8 <sup>th</sup> $ ho_{e^-}$ Fe |
|------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| CMF        | 740                              | 648                              | 555                              | 463                              |
| C SRC      | 230                              | 201                              | 173                              | 144                              |
| Fe MF      | 0                                | 90                               | 180                              | 270                              |
| Fe SRC     | 0                                | 28                               | 56                               | 84                               |

# Scenario 2: Replace 1/8<sup>th</sup> total e<sup>-</sup> density with Pb

# Lead Target Thickness: $\frac{1.26 E24 e^{-}/cm^{2}}{8} \cdot \frac{1}{2.69 E24 e^{-}/cm^{3}} = 586 \,\mu\text{m}$ 586 µm · 11.35 $\frac{g}{cm^3}$ · $\frac{mole}{208 g}$ · $\frac{6E23}{mole}$ = 1.9E21 cm<sup>-2</sup> • $R_{Pb}^{MF} = \frac{740}{day} \cdot \frac{1.9E21}{1.45E23} \cdot \frac{126}{6} \cdot \frac{0.17}{0.44} = 79/day$ • $R_{Pb}^{SRC} = \frac{230}{day} \cdot \frac{1.9E21}{1.45E23} \cdot \frac{126}{6} \cdot \frac{0.17}{0.44} = 24/day$

# Summary of Lead Scenarios

#### Events per day

| Event Type | 0/8 <sup>th</sup> $ ho_{e^-}$ Pb | 1/8 <sup>th</sup> $ ho_{e^-}$ Pb | 2/8 <sup>th</sup> $ ho_{e^-}$ Pb | 3/8 <sup>th</sup> $ ho_{e^-}$ Pb |
|------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| CMF        | 740                              | 648                              | 555                              | 463                              |
| C SRC      | 230                              | 201                              | 173                              | 144                              |
| Pb MF      | 0                                | 79                               | 158                              | 237                              |
| Pb SRC     | 0                                | 24                               | 48                               | 72                               |